Modeling diverse physics of nanoparticle self-assembly in pulsed laser-irradiated metallic films

Mikhail Khenner

Department of Mathematics and Computer Science, Western Kentucky University

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Outline

- Motivation for modeling, challenges
- Single layer films
 - Model description
 - Lubrication and 2D approximations
 - (i) Uniform irradiation: Stability analysis
 - (ii) Computations of the nonlinear dynamics of the film
- Bilayer films
 - (i) Model equations (2D)
 - (ii) Stability analysis, simulations
- Future work

IDewetting ≡ "uncovering" (exposure) of some areas the substrate



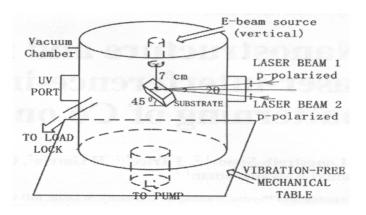
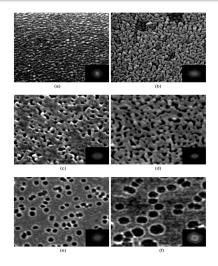


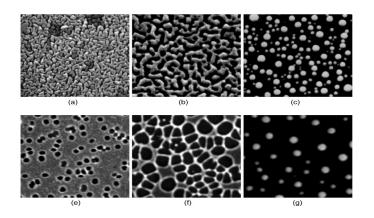
Figure courtesy of R. Kalyanaraman, UTK

Single-layer films, one laser beam: Morphologies in the early stages of dewetting



Irradiation by 10 laser pulses. Ag film thickness from (a) to (f): 2, 4.5, 7.4, **9.5**, **11.5**, 20 nm. (Figure courtesy of R. Kalyanaraman, UTK)

Single-layer films, one laser beam: Progression of dewetting towards formation of nanoparticles



Top row: 4.5 nm thick Ag film. (a)-(c): 10, 100, 10500 laser pulses. Bottom row: 11.5 nm thick Ag film. (e)-(g): 10, 100, 10500 laser pulses. (Figure courtesy of R. Kalyanaraman, UTK)

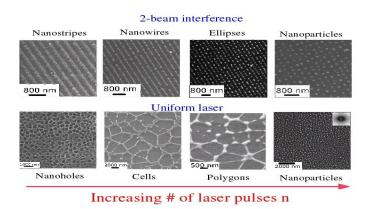
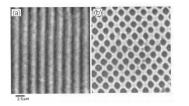


Figure courtesy of R. Kalyanaraman, UTK

Laser interference irradiation



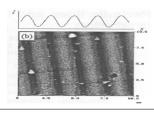
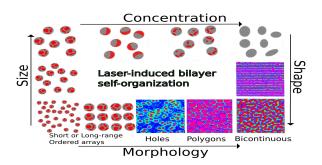


Figure:

Left: Micrographs of 1D and 2D optical interference gratings created on a Au film of 18 nm thickness. (a) "two-beam" and (b) "four-beam" gratings.

Right: AFM image of 8 nm Au film after two-beam interference irradiation. Note that film material accumulates in cold regions. (From Y. Kaganovskii *et al.*, JAP 100, 044317, 2006)

Vision of a multifunctional nanostructured surface platform based on multi-layer films



Pulsed laser self-organization of multilayer films made from immiscible materials, like Co and Ag, can be used to synthesize a matrix of discrete micro-regions with varying nanoscale morphology, size, shape, and composition. Thus a platform with unique multifunctional behavior for sensing and detection can be made. (Figure courtesy of R. Kalyanaraman, UTK)

Challenges:

- Understand film instabilities resulting in nanopatterning
- Develop a realistic model of heat transfer within the film
- Develop a model of interference control of a pattern formation
- For bilayers, develop models that account for interdiffusion and chemical reactions
- Develop efficient computational methods for 3D simulations (especially for a bilayer system)

Our interest is to model the complete dewetting cycle - from a continuous film to a nanoparticles state

Modeling assumption

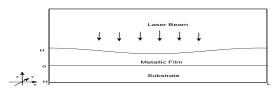
Film is liquid at all times, and dewetting is modeled as continuous in time.

In reality, pulse width =10 ns, pulse frequency =50 Hz. Nanometer-scale film is:

- Melted "instantaneously" when a pulse hits (energy flux $\sim 10^{11} \text{ J/s} m^2$);
- Dewets while the pulse lasts;
- Solidifies "instantaneously" after the pulse is gone, freezing the instantaneous morphology;
- Next pulse quenches in the morphology and the cycle repeats.



Single layer films



Major physical factors contributing to pattern formation through film dewetting:

- Capillary fluid flow (minimization of the surface area at given fluid volume by the surface tension)
- Unusual, thickness-dependent heat transfer in the film due to nonlinear optical absorption of light and nonlinear reflectivity
- Thermocapillary (Marangoni) fluid flow arising due to the surface tension dependence on temperature
- Long-range intermolecular (van der Waals) forces between the substrate and film surface molecules



Important facts

- Molten metal is an incompressible Newtonian liquid.
- Surface tension decreases linearly with increasing temperature

$$\sigma = \sigma_m - \gamma (T - T_m), \quad T > T_m, \quad \gamma > 0$$

• $H/L = \epsilon \ll 1$, also $H_s \sim 10 \div 20 H \rightarrow$ will derive model equations in the lubrication (longwave) approximation.

Lubrication approximation is, essentially, a procedure of systematic scalings of governing equations (Navier-Stokes) and expansion of all fields in powers of small parameter ϵ . Lubrication equations are the equations that result in the leading zeroth-order (ϵ^0) of such expansion (Oron, Davis, and Bankoff, *Reviews of Modern Physics* (1997); Craster and Matar, *Reviews of Modern Physics* (2009)).



Lubrication approximation: leading-order expansion in ϵ (<< 1)

Momentum equation (Stokes) and continuity equation

$$\nabla \cdot \mathbf{\Omega} + \rho \mathbf{g} = 0, \quad \nabla \cdot \mathbf{u} = 0 \tag{1}$$

Energy equation

$$\frac{\kappa}{\rho c_p} \nabla^2 T + Q = 0, \tag{2}$$

where

$$\mathbf{\Omega} = -P\delta_{ij} + \eta \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right)$$
 : stress tensor

$$Q = \frac{\delta J(1 - R(h))}{2} f(x, y, t) \exp(\delta(z - h)) \quad \text{(Beer-Lambert law)}$$
$$(0 \le R(h) < 1 : \text{nonlinear reflectivity)}$$

Remark 1: Nonuniformity in the plane of the film enters through

$$f(x, y, t)$$
.

At the free surface:

(i) The normal and shear stress balances;

$$\mathbf{n} \cdot \mathbf{\Omega} \cdot \mathbf{n} = -\sigma \nabla \cdot \mathbf{n} + \Pi, \quad \mathbf{t} \cdot \mathbf{\Omega} \cdot \mathbf{n} = \mathbf{t} \cdot \nabla \sigma$$

where $\Pi = (A/6\pi)h^{-3}$ is the **disjoining pressure** due to long-range intermolecular attraction

- (ii) The kinematic condition: $u_3 = h_t + u_1 h_x + u_2 h_y \leftarrow$ this condition is used to derive the evolution PDE for h after u_1 an u_2 have been averaged in the z-direction
- (iii) Newton's law of cooling: $\kappa T_z = -\alpha_h (T T_a)$



Boundary conditions (II)

At the film-substrate interface:

- No-slip: $u_1 = u_2 = 0$
- No-penetration: $u_3 = 0$
- Continuity of temperature and thermal flux:

$$T = \theta, \quad \kappa T_z = \kappa_s \theta_z,$$
 (3)

where θ is the temperature field in the substrate, which is obtained by solving the heat conduction equation

$$\frac{\kappa_s}{\rho_s c_{ps}} \nabla^2 \theta + Q = 0 \tag{4}$$

given R(h)=0 in the optically transparent substrate (such as SiO_2) and the boundary condition $z=-H_s$: $\theta=T_s$



Temperature profiles

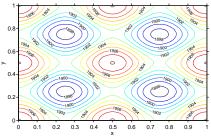


Figure: Surface temperature when four-beam interference is active, modeled by $f \equiv f(x, y) = 1 + 0.1 \cos(4\pi(x - 1/2)) \cos(4\pi(y - 1/2))$

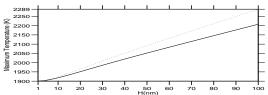


Figure: Plot of the maximum film temperature vs. film height. Dot curve: R(h) = 0; solid curve: $R(h) = r_0 (1 - \exp(-a_r h))$.

2D evolution equation (dimensionless) for the film height h(x, t)

$$h_{t} = \frac{\partial}{\partial x} \left[-(C/3)h^{3}h_{xxx} + (G/3)h^{3}h_{x} - Ah^{-1}h_{x} \right. \\ \left. + M\beta(T_{a} - T_{s})h^{2}h_{x} \right. \\ \left. + \left\{ -MF_{h}(1 - R(h)) + MR'(h)F - M\beta(h + \Psi)R'(h)F + M\beta(1 - R(h)) \left(F + (h + \Psi)F_{h}\right)\right\} f(x, y, t)h^{2}h_{x} \right]$$

Lines 3 and 4: unconventional terms that emerge due to laser heating

C: capillary numer, G: gravity number, β : Biot number, M: Marangoni number, T_a : ambient temperature, T_s : substrate temperature, A: Hamaker constant, $D = \delta H$: optical thickness, $\Psi = H_s/H\Gamma$, where $\Gamma = \kappa/\kappa_s$

$$R(h) = r_0 (1 - \exp(-a_r h)),$$

 $F(h, D, \Psi) = (-\Psi + \exp(-Dh)(\Psi - 1/D) - h + 1/D)/2$



Linear stability analysis (note: irradiation is uniform in space, time) (I)

Take f=1, $h=1+\xi(x,t)=1+e^{\omega t}\cos kx$ and linearize in ξ :

$$\omega(k) = -\frac{G}{3}k^{2} - \frac{\epsilon^{3}}{3C}k^{4} + Ak^{2} - M\beta(T_{a} - T_{s})k^{2} + MR'F(-1 + \beta(1 + \Psi))k^{2} + M(1 - R)(F_{h} - \beta(F + (1 + \Psi)F_{h}))k^{2}.$$
(5)

h = 1: Dimensionless film height at t = 0

 $\xi(x,t)$: Small perturbation

 ω : Growth rate of the perturbation

k : Wavenumber of the perturbation (wavelength $= 2\pi/k$)

 R, R', F, F_h are evaluated at h = 1



Linear stability analysis (II)

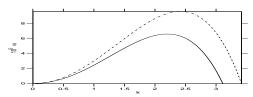


Figure: Variation of ω with k: Dash-dot curve: heat source is zero; solid curve: heat source is non-zero.

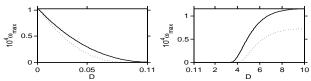


Figure: Variation of ω_{max} with D. Dot curve: R(h) = 0; solid curve:

 $R(h) \neq 0$.

Thé uniformly heated film is completely stable against small perturbations in some interval of the optical thickness parameter

Computation of a nonlinear evolution of the film (I)

Single laser beam (no interference, i.e. f = 1):

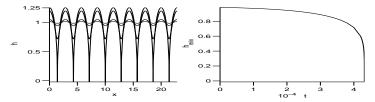


Figure: Profile of the film height (left), and the evolution of the minimum point on the film surface (right). Note the formation of a nanowire array. Spacing equals $2\pi/k_{max} \equiv$ wavelength of the fastest growing perturbation ($\omega = \omega_{max}$).

Rupture time $T_r \approx 0.9$ ms (depends on the amplitude of the initial film height).



Computation of a nonlinear evolution of the film (II)

Two-beam interference: $f \equiv f(x) = 1 + 0.99 \cos(0.157(x - \frac{\pi}{2.2}))$ Note: $2\pi/0.157 = 40$: the distance between interference fringes

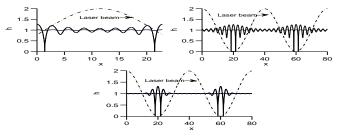


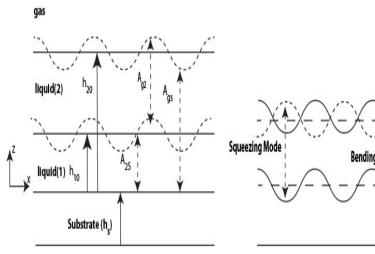
Figure: Top row, left: H=10 nm, 8 wavelengths; Top row, right: H=10 nm, 28 wavelengths; Bottom row: H=15 nm, 28 wavelengths.

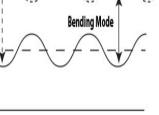
The spatial periodicity of nanowires follows the interference imprint.



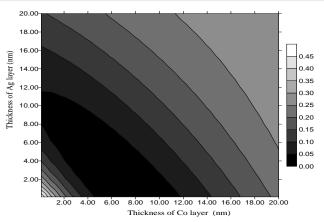
Bilayer films (Interference not included yet; 2D analysis)

Problem geometry: bilayer + transparent SiO_2 substrate + reflective support layer





Reflectivity (shown: AgCo bilayer, model)



 $R = R(h_1, h_2 - h_1)$ is a smooth convex function of its arguments; model adapted from J.S.C. Prentice, "Coherent, partially coherent and incoherent light absorption in thin-film multilayer structures," J. Phys. D: Appl. Phys. **33**, 3139 (2000).

2D lubrication equations for layers thicknesses (Pototsky et al. (2005))

$$\begin{array}{lll} \partial_t h_1 + \partial_x \left[F_{11} \partial_x P_1 + F_{12} \partial_x P_2 + \Phi_{11} \partial_x \sigma_1 + \Phi_{12} \partial_x \sigma_2 \right] & = & 0, \\ \partial_t h_2 + \partial_x \left[F_{21} \partial_x P_1 + F_{22} \partial_x P_2 + \Phi_{21} \partial_x \sigma_1 + \Phi_{22} \partial_x \sigma_2 \right] & = & 0, \end{array}$$

 $F_{\ell m}\left(h_1,h_2-h_1\right)$ and $\Phi_{\ell m}\left(h_1,h_2-h_1\right)$ are polynomials of a degree at most three, and $\sigma_i=\sigma_i\left(T_i\left(h_i(x,t)\right)\right)$ (next slide)

Pressures:

$$P_{1} = -\sigma_{1}\partial_{xx}h_{1} - \sigma_{2}\partial_{xx}h_{2} + \Pi_{1} + \Pi_{2} + \rho_{1}gh_{1} + \rho_{2}g(h_{2} - h_{1}),$$

$$P_{2} = -\sigma_{2}\partial_{xx}h_{2} + \Pi_{2} + \rho_{2}gh_{2},$$

Disjoining pressures:

$$\begin{split} \Pi_{1}\left(h_{1},h_{2}-h_{1}\right) &=& \frac{A_{s2}}{h_{1}^{3}}-\frac{A_{g2}}{\left(h_{2}-h_{1}\right)^{3}}+\frac{S_{1}\exp\left(-\frac{h_{1}}{\ell_{1}}\right)}{l_{1}}-\frac{S_{2}\exp\left(-\frac{\left(h_{2}-h_{1}\right)}{\ell_{2}}\right)}{l_{2}},\\ \Pi_{2}\left(h_{1},h_{2}-h_{1}\right) &=& \frac{A_{g2}}{\left(h_{2}-h_{1}\right)^{3}}+\frac{A_{sg}}{h_{2}^{3}}+\frac{S_{2}\exp\left(-\frac{\left(h_{2}-h_{1}\right)}{\ell_{2}}\right)}{l_{2}}. \end{split}$$

Energy equations:

$$\begin{split} \frac{\kappa_{1,2}}{\rho_{1,2} C_{\text{eff}}} \partial_{zz} T_{1,2} + \frac{\delta_2}{\rho_{1,2} C_{\text{eff}}} J\left(1-R\right) \exp\left(\delta_{1,2} \left(z-h_2\right)\right) &= 0, \\ \frac{\kappa_s}{\rho_s C_{\text{eff}}} \partial_{zz} T_s &= 0. \end{split}$$

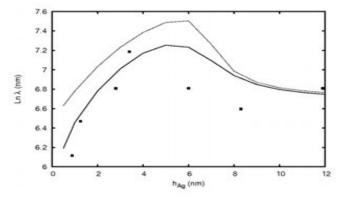
(Add physical boundary conditions on all three intefaces and solve using CAS)

Surface tensions decrease linearly with increasing temperature:

$$\begin{split} \sigma_1 &= \sigma_1^{(m)} - \gamma_1 \left(T_1 \left(z = h_1 \right) - T_1^{(m)} \right), \quad \gamma_1 > 0, \ T_1 \left(z = h_1 \right) > T_1^{(m)}, \\ \sigma_2 &= \sigma_2^{(m)} - \gamma_2 \left(T_2 \left(z = h_2 \right) - T_2^{(m)} \right), \quad \gamma_2 > 0, \ T_2 \left(z = h_2 \right) > T_2^{(m)}, \end{split}$$

Interwire spacing λ from the linear stability analysis of Ag/Co bilayer

Co thickness = 5 nm fixed, Ag thickness varies

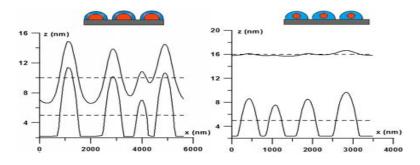


Solid squares: experimental points; Solid line: nonisothermal model; dashed line: isothermal model ($T_i = const.$, $\sigma_i = const.$, thus no thermocapillary (Marangoni) effect)

Simulation of the full nonlinear PDE system for Ag/Co bilayer

Co thickness = 5 nm fixed, Ag thickness = 5 nm (left), = 11 nm (right)

Evolves in bending mode



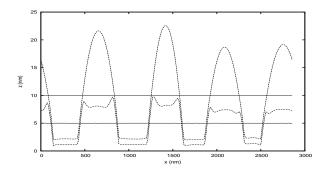
Core-shell wires

Embedded wires



Simulation of the full nonlinear PDE system for Co/Ag bilayer

Outcomes as for AgCo (*core-shell, embedded*), and also *stacked* Evolves in bending mode



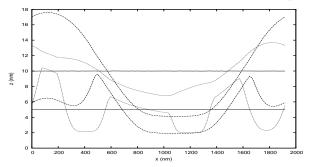
Stacked wires



Squeezing mode: wires do not form

Tentatively, only the bending mode of evolution results in practically useful outcomes, such as core-shell, embedded, or stacked.

We derived criterium for mode type in the linear regime (small t).



Squeezing mode



Future Work

- Inclusion of interference (bilayer model)
- Inclusion of interdiffusion and chemical reactions (bilayer model)
- Development of the efficient FD code for 3D simulations

Publications:

- A. Atena and M. Khenner, "Thermocapillary effects in driven dewetting and self-assembly of pulsed laser-irradiated metallic films", Phys. Rev. B 80, 075402 (2009)
- Wh. Krishna, R. Sachan, J. Strader, C. Favazza, M. Khenner, and R. Kalyanaraman, "Thickness-dependent spontaneous dewetting morphology of ultrathin Ag films", Nanotechnology 21, (2010) 155601
- M. Khenner, S. Yadavali, and R. Kalyanaraman, "Formation of organized nanostructures from unstable bilayers of thin metallic liquids" (submitted)